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S/200/61/000/001/001/005
D223/D305

Determination of inertia...

a) для случая $w_1 > w_2$

Без сопр.

$$R_1 = \frac{S_1}{\tau_1} = \left(\frac{\tau_2}{\tau_1} - 1 \right) T_1,$$

б) для случая $w_1 < w_2$

$$R_2 = \frac{S_2}{\tau_2} = \left(\frac{\tau_1}{\tau_2} - 1 \right) T_2,$$

в) для случая $w_1 = w_2$

$$R = 0.$$

where w_1 and w_2 = flow rates of media. The last case ($w_1 = w_2$) has pure retardation as $S = 0$. This case, state the authors, is best for use in solving the control problem. By means of nomograms given above, values of T_1 , T_2 can be found and their change with the change of parameters could be used in constructing the exchanger for most efficient and economical processing. Such a case is governed by $F(\alpha, \beta) = 0$, and the connection between α and β is given by the quantity P as defined by:

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$$\rho = 1 - m = \frac{\epsilon(1 - e^{-\epsilon})}{\epsilon + \beta_0} \quad (16)$$

In order to check theoretical deductions the authors give the results of practical work and state that these results agreed well with (8), (12) and (14). The article contains a short list of symbol values: μ_1, μ_2 - temperature of the first and second media; ν - temperature of the dividing wall; x_1 - heat exchanger coordinate section, calculated in the direction of the first medium's movement; w_1, w_2 - speed of media movement; k_1, k_2, k_3, k_4 - proportionality coefficients of temperature changes; ρ_1 - boundary perimeter of interface of wall and first medium; ρ - differentiating operator; ρ_2 - boundary perimeter of interface of wall and second medium; k_1, k' - heat transfer coefficients; S_3 - cross section area of dividing wall; γ_3 - specific gravity of wall; C_3 - heat capacity of wall. There are 3 figures and 3 Soviet-bloc references.

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ASSOCIATION: Institut avtomatiki i elektrometrii Sibirskogo otdeleniya AN SSSR (Institute of Automation and Electrometry, Siberian Section, AS USSR)

SUBMITTED: April 4, 1960.

Card 12/12

S/200/61/000/008/001/004
D218/D306

26.5200

AUTHORS: Devyatov, B.N., and Khor'kova, G.S.

TITLE: Inertia and regulation of counterflow heat exchangers with variable-speed heat carriers

PERIODICAL: Akademiya nauk SSSR. Izvestiya. Sibirskoye otdeleniye, no.8, 1961, 36 - 43

TEXT: In previous papers the first of the present authors and Yu.N. Kornev (Ref 1: Tr. In-ta avtomatiki i elektrometrii, SO, AN SSSR, no. 2, 1960) and S.V. Lapshin (Ref 2: Tr. In-ta avtomatiki i elektrometrii, SO, AN SSSR, no. 2, 1960) discussed the transfer functions for heat exchangers of the "tube in tube" type and discussed their inertia and regulation under steady-state conditions. It was assumed that the velocity of the heat carriers was constant. In reality, the velocity is a random function of time and hence a steady-state theory cannot be used. These and other considerations necessitate the study of the dynamic properties of such heat exchangers. The set of equations which describes nonsteady state processes in a counterflow heat exchanger is of the form Eq. (1)

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$$\left\{ \begin{array}{l} \frac{\partial u_1}{\partial t} + w_1 \frac{\partial u_1}{\partial x} = \chi_1 (u_2 - u_1), \\ \frac{\partial u_2}{\partial t} - w_2 \frac{\partial u_2}{\partial x} = \chi_2 (u_1 - u_2), \end{array} \right. \quad (1)$$

where U_1 and U_2 is the temperature of the two moving media in the heat exchanger respectively, w_1 and w_2 are the linear velocities, and χ_1, χ_2 , are coefficients describing the heat exchange between the two media. Since the velocity is an arbitrary function of time, these equations have variable coefficients and their general solution is difficult to obtain. The transfer functions for the problem may be found in two ways. Firstly, one can determine the solution for a step-change in the velocity, and secondly, one can obtain an approximate representation of Eq. (1) by a nonhomogeneous system with constant coefficients. The present authors show that the first method does not lead to the required transfer function but leads to a rather inconvenient formula which is a nonlinear function of the velocity change. It is, therefore, concluded that it is of doubtful value for practical purposes. A simpler, and linear, transfer function can be obtained by the second of

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the above two methods. When the steady-state conditions are disturbed, i.e. when there is a change in the velocity, Eq. (1) assumes the form -Eq. (6)-

$$\left\{ \begin{array}{l} \frac{\partial(u_{10} + \Delta u_1)}{\partial t} + (w_1 + \Delta w_1) \frac{\partial(u_{10} + \Delta u_1)}{\partial x} = \chi_1 [(u_{20} + \Delta u_2) - \\ \quad - (u_{10} + \Delta u_1)], \\ \frac{\partial(u_{20} + \Delta u_2)}{\partial t} - (w_2 + \Delta w_2) \frac{\partial(u_{20} + \Delta u_2)}{\partial x} = \chi_2 [(u_{10} + \Delta u_1) - \\ \quad - (u_{20} + \Delta u_2)], \end{array} \right. \quad (6)$$

where u_{10} and u_{20} are the steady-state values of the temperature of the first and second media at $t=0$. The equations representing the steady-state conditions are of the form -Eq. (7)-

$$\left\{ \begin{array}{l} \frac{\partial u_{10}}{\partial t} + w_1 \frac{\partial u_{10}}{\partial x} = \chi_1 (u_{20} - u_{10}), \\ \frac{\partial u_{20}}{\partial t} - w_2 \frac{\partial u_{20}}{\partial x} = \chi_2 (u_{10} - u_{20}), \end{array} \right. \quad (7)$$

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where $\frac{\partial u_{10}}{\partial t} = 0 = \frac{\partial u_{20}}{\partial t}$. Subtracting Eq. (7) from Eq. (6) one obtains the following two equations:

$$\left\{ \begin{array}{l} \frac{\partial u_1}{\partial t} + w_1 \frac{\partial u_1}{\partial x} + \Delta w_1(t) \frac{\partial u_{10}}{\partial x} + \Delta w_1(t) \frac{\partial u_1}{\partial x} = \chi_1 (u_2 - u_1), \\ \frac{\partial u_2}{\partial t} - w_2 \frac{\partial u_2}{\partial x} - \Delta w_2(t) \frac{\partial u_{20}}{\partial x} - \Delta w_2(t) \frac{\partial u_2}{\partial x} = \chi_2 (u_1 - u_2). \end{array} \right.$$

Assuming that $\Delta w(t)$ are small and neglecting $\Delta w_1(t) \frac{\partial u_1}{\partial x}$ and $\Delta w_2(t) \frac{\partial u_2}{\partial x}$, one obtains the following differential equations with constant coefficients-Eq. (8)-

$$\left\{ \begin{array}{l} \frac{\partial u_1}{\partial t} + w_1 \frac{\partial u_1}{\partial x} = \chi_1 (u_2 - u_1) - \Delta w_1(t) \frac{\partial u_{10}}{\partial x}, \\ \frac{\partial u_2}{\partial t} - w_2 \frac{\partial u_2}{\partial x} = \chi_2 (u_1 - u_2) + \Delta w_2(t) \frac{\partial u_{20}}{\partial x}. \end{array} \right. \quad (8)$$

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This set of equations will hold only in the case of small perturbations. The solution may be found with the aid of the operator method subject to the following boundary conditions: . . .

$$u_1(x_1, 0) = 0, \quad u_2(x_1, 0) = 0,$$

$$u_1(0, t) = u_1(t), \quad u_2(1, t) = u_2(t).$$

The final transfer function is then found to be - Eq. (9) -

$$K_{11} = \bar{K}_{11} C a_1 \frac{\frac{1}{p\tau_1 + a_1 + \lambda_1} \frac{1 - e^{(\alpha_1 - \alpha_2 + \lambda_1)t}}{\alpha_1 - \alpha_2 + \lambda_1} - \frac{1}{p\tau_1 + a_1 + \lambda_2} \frac{1 - e^{(\alpha_1 - \alpha_2 + \lambda_2)t}}{\alpha_1 - \alpha_2 + \lambda_2}}{\frac{1}{p\tau_1 + a_1 + \lambda_1} - \frac{1}{p\tau_1 + a_1 + \lambda_2}}, \quad (9)$$

where -

$$\bar{K}_{11} = \frac{(\lambda_1 - \lambda_2) e^{\lambda_1 t} + \lambda_2}{(\lambda_1 + p\tau_1 + a_1) e^{\lambda_1 t} - (\lambda_2 + p\tau_1 + a_1) e^{\lambda_2 t}};$$

$$a_1 = \frac{x_1 l}{w_1}; \quad a_2 = \frac{x_2 l}{w_2};$$

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and C is the temperature difference between the first and second media at the output of the apparatus in steady-state conditions. The above transfer function is convenient both for studying the dynamic properties of heat exchangers and also in practical calculations concerned with control problems. A consideration of the transfer functions obtained in this way shows that when there is a change in the velocity and the steady-state conditions are thus upset, the transient process at the output begins instantaneously, i.e. there is no delay, which is consistent with the physical interpretation of the problem. It follows that the operation of the heat exchanger may be better controlled by adjusting the velocity of one of the media rather than by adjusting the temperature. In practice, it is convenient to define the inertia of the heat exchanger. The inertia is numerically equal to the area between the transient process curve and the straight line corresponding to the new steady state conditions, i.e. - .

$$I = \frac{1}{m} \int_0^\infty [m - u_1(t)] dt ,$$

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where m is temperature in the new steady-state conditions. The inertia can also be expressed in terms of the transfer function Ref 1.):

$$I = - \lim_{p \rightarrow 0} [1nK_{11}]'. \quad (10)$$

A further useful quantity is the dimensionless inertia which may be defined by

$$S = \frac{I}{\tau_1 + \tau_2}.$$

Since the transient process in this case occurs immediately, i.e. there is no delay, the inertia is also a measure of the regulation. Using the linear transfer function given by Eq. (9), it is found that the inertia is given by - Eq. (11) -

$$S = S_1 + \alpha_1 \alpha_2 \frac{2(\alpha_1 - \alpha_2) - \frac{(\alpha_1 - \alpha_2)^2}{2} - 3 + e^{\alpha_1 - \alpha_2} (3 + \alpha_1 - \alpha_2)}{(\alpha_1 - \alpha_2)^2 [\alpha_1 (\alpha_1 - \alpha_2) - \alpha_2 (1 - e^{\alpha_2 - \alpha_1})]} +$$

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$$+ \tau_1' \frac{\frac{\alpha_2}{\alpha_1 - \alpha_2} - \frac{\alpha_1(\alpha_1 - \alpha_2)}{2} - e^{\alpha_2 - \alpha_1} \left[\frac{\alpha_2}{\alpha_1 - \alpha_2} + \alpha_2 \right]}{\alpha_1(\alpha_1 - \alpha_2) - \alpha_2(1 - e^{\alpha_2 - \alpha_1})}, \quad (11)$$

where

$$\tau_1' = \frac{\tau_1}{\tau_1 + \tau_2},$$

and S_1' is the inertia when the temperature of the first medium is disturbed, and is given by

$$S_1' = \alpha_1 \alpha_2 \frac{(\alpha_1 - \alpha_2)(1 - e^{\alpha_2 - \alpha_1}) - 2(1 - e^{\alpha_2 - \alpha_1})}{(\alpha_1 - \alpha_2)^2 (\alpha_1 - \alpha_2 e^{\alpha_2 - \alpha_1})} + \tau_1'. \quad \text{H}$$

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The above formula gives the inertia of the transient process in the heat exchanger as a function of its parameters α_1 , α_2 , and τ_1' . Fig. 2 shows the curves of equal inertia. This figure is convenient in the selection of the optimum control conditions. However, the values of the parameters which correspond to the optimum control conditions do not always ensure that the apparatus will work satisfactorily in other respects. Fig. 3 shows typical plots of curves of equal inertia for given values of τ_1' . Other figures reproduced may be used to determine the inertia for any values of α_1 , α_2 , τ_1' . In this way, the authors obtain a set of graphs which describe the change in the inertia as a function of the parameters of the heat exchangers. These may be used to select the optimum parameters for control purposes. There are 8 figures and 3 Soviet-bloc references.

ASSOCIATION: Institut avtomatiki i elektrometrii Sibirskego otdeleniya AN SSSR, Novosibirsk (Institute of Automation and Electrometry of the Siberian Branch AS SSSR, Novosibirsk)

SUBMITTED: February 7, 1961

Card 9/10

DEVYATOV, B.N.; GIMEL'SHTEYN, F.Ya.

Equation for the interaction of moving media in technological apparatus taking into consideration the influence of the thermal effect of the chemical reaction. Izv. Sib. otd. AN SSSR no. 3:12-20 '61. (MIRA 14:5)

1. Institut avtomatiki i elektrometrii Sibirskogo otdeleniya AN SSSR, Novosibirsk.
(Chemical reactions, Heat of)

24.5200

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S/200/61/000/009/001/003
D219/D301

AUTHORS: Devyatov, B.N., and Kornev, Yu.N.

TITLE: Determination of transients in continuously operating heat-exchangers

PERIODICAL: Akademiya nauk SSSR. Sibirskoye otdeleniye Izvestiya, no. 9, 1961, 21-27

TEXT: The errors in approximate representation of transient processes can be evaluated from experimental data. The lack of exact theoretical expressions does not permit, however, determining the origin and, therefore, the meaning of these errors. In the present article, the authors determine exact integral curves and solve the differential equations for the heat exchange which permit exact calculation of the transient for a unit pulse input in the same type of heat exchanger. Under the same assumptions and using the same notation the initial differential equations are

$$\frac{\partial u_1}{\partial t_1} + w_1 \frac{\partial u_1}{\partial x_1} = k_1 (u_2 - u_1),$$

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$$\frac{\partial u_2}{\partial t_1} + w_2 \frac{\partial u_2}{\partial x_1} = k_2 (u_1 - u_2), \quad (1)$$

where u_1 , u_2 - temperatures of the 1st and 2nd medium respectively, k_1 , k_2 - proportionality factors of temperature change, x_1 - the coordinate of the cross section of the instrument in the direction of the 1st medium movement t_1 - time in seconds. The same equation (1) in dimensionless complex parameters has the form of

$$\tau_1 \frac{\partial u_1}{\partial t} + \frac{\partial u_1}{\partial x} = \alpha (u_2 - u_1),$$

$$\tau_2 \frac{\partial u_2}{\partial t} + \frac{\partial u_2}{\partial x} = \beta (u_1 - u_2), \quad (2)$$

where

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$$\alpha = \frac{k_1 l}{w_1}, \quad \beta = \frac{k_2 l}{w_2}, \quad x = \frac{x_1}{l},$$

$$t = \frac{t_1}{|\bar{\tau}_1' - \bar{\tau}_2'|}, \quad \bar{\tau}_1' = \frac{\bar{\tau}_1'}{|\bar{\tau}_1' - \bar{\tau}_2'|}, \quad \bar{\tau}_2' = \frac{\bar{\tau}_2'}{|\bar{\tau}_1' - \bar{\tau}_2'|},$$

in which

$\bar{\tau}_1' = \frac{1}{w_1}; \quad \bar{\tau}_2' = \frac{1}{w_2};$ where l .. length of the heat exchanger and
 $t = \frac{t_1}{\bar{\tau}_1' + \bar{\tau}_2'};$ the transient is assumed to exist at the output with a
 temperature at the input being u_1 and the problem is solved in all cases
 for the zero condition. $u_1(0, x) = 0, u_2(0, x) = 0.$ With the counter flow
 present Eq. (2) takes the form of Eq. (3)

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$$\begin{aligned} \tilde{\tau}_1 \frac{\partial u_1}{t} + \frac{\partial u_1}{x} &= \alpha (u_2 - u_1), \\ \tilde{\tau}_2 \frac{\partial u_2}{\partial t} - \frac{\partial u_2}{\partial x} &= \beta (u_1 - u_2), \end{aligned} \quad (3)$$

with the boundary conditions $u_1(t, 0) = 1$, $u_2(t, 1) = 0$. Because of the series structure the solution for any number of terms can be taken, with the exact solution obtained every time within the interval $(\tilde{\tau}_1, \tilde{\tau}_1 + n+1)$. The subsidiary solution is obtained first as Eq. (7)

$$F_1(p) \approx f_1(t) = \frac{d}{dt} \varphi(t) - a^2 \int_0^t \varphi(t) dt, \quad (7)$$

$$\text{where Eq. 7a } \varphi(t) = \frac{t^{2n+1} I_{2n+1}(T)}{T^{2n+1}}, \quad T^2 = a^2 [t^n + (2n+1)t].$$

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(In it symbol $\hat{=}$ denotes the correspondence between the rendering and the original and $I(T)$ - Bessel function of the given order). Applying to Eq.(6) the perturbation theorem and considering Eq.(7) the final expression for the transient u_1 in the original is obtained as

$$u_1 = u_1(t) = 2 \sum_{n=0}^{\infty} (4\alpha\beta)^n \cdot e^{-[(n+1)\alpha + n\beta]} \cdot \eta(\tau) [e^{-(\alpha+\beta)\tilde{T}} f(\tau) + \\ + (\alpha+\beta) \int_0^{\tilde{T}} e^{-(\alpha+\beta)\tilde{\tau}} \cdot f(\tau) d\tilde{\tau}], \quad (8)$$

where

$$\tilde{T} = t - \frac{1}{\alpha} - n, \quad f(t) = \frac{d}{dt} \varphi(t) - 4\alpha\beta \int_0^t \varphi(t) dt, \\ \varphi(t) = \frac{t^{2n+1} I_{2n+1}(t)}{T^{2n+1}}, \quad T = \sqrt{4\alpha\beta[t^2 + (2n+1)t]},$$

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and $\eta(\tau)$ - a unit function with delay $\bar{\tau}_1 + n$. The experimental curve of the transient was obtained from a model heat exchanger with counter flow, for which $\alpha = 2.074$, $\beta = 1.294$, $\bar{\tau}_1 = 18.38$ sec; $\bar{\tau}_2 = 11.55$ sec. the first term of series (8) has the form

$$u_{10} = 2e^{-\alpha} \eta(\tau) e^{-(\alpha+\beta)\tau} \cdot \varphi(\tau) + (\alpha + \beta) \int_0^{\bar{\tau}} e^{-(\alpha+\beta)t} \varphi(t) dt ,$$

where

$$\varphi(t) = 1 - \frac{I_0(T)}{2(t+1)} - \frac{t}{t+1} \frac{I_1(T)}{T} + 2\alpha\beta \int_0^t \frac{I_1(T)}{T} dt.$$

Comparison of the integral curve with that of the transient obtained from the experiment is shown

The experimental curve was obtained using a model of indirect flow heat exchanger for which $\alpha = 3.794$, $\beta = 1.931$, $\bar{\tau}_1 = 45.09$ sec. $\bar{\tau}' = 22.67$ sec. The divergences between the theoretical and experimental curves in both graphs are due to the fact that in the basic equations, mixing between

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Determination of transients ...

the media and heat exchange through the walls was neglected. There are 3 figures and 3 Soviet-bloc references

ASSOCIATION: Institut avtomatiki i elektrometrii Sibirskogo otdeleniya AN SSSR, Novosibirsk
(Institute of Automation and electrometry of the Siberian Department, AS USSR, Novosibirsk)

SUBMITTED: February 17, 1961

Card 7/7

DEVYATOV, B.N.

Determination of the inertness and control system of
technological process designs. Dokl. AN SSSR 141 no.5:1151-1154
D '61. (MIRA 14:12)

1. Institut avtomatiki i eletrometrii Sibirskogo otdeleniya
AN SSSR. Predstavлено академиком V.S. Kulebakиным.
(Automatic control)

DEVYATOV, B.N. (Novosibirsk); KORNEV, Yu.N. (Novosibirsk)

Determination of the transfer functions of objects with
monotonic limited characteristics. Izv. AN SSSR. Otd. tekhn.
nauk. Energ. i avtom. no.1:169-176 Ja-F '62. (MIRA 15:3)
(Automatic control)

S/200/62/000/005/001/005
I042/I242

AUTHORS: Devyatov, B.N. and Kornev, Yu. N.

TITLE: Application of the Burman-Lagrange series to
the analysis of transient chemical engineering
processes

PERIODICAL: Akademiya nauk SSSR. Sibirskoye otdeleniye.
Izvestiya, no.5, 1962, 14-28

TEXT: The characterization of transient processes often
requires the analysis of systems of equations containing partial
derivatives. Generally, it is not expedient to seek an exact sol-
ution because the corresponding functions are transcendental. Such
systems can be solved indirectly, in the form of convergent Burman-

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Lagrange series. The latter are obtained by decomposition of an analytical function $F(p)$ in terms of another function $\omega(p)$

$$F(p) = \sum_{n=0}^{\infty} d_n [\omega(p)]^n \quad (1)$$

The coefficients d_n are obtained by expansion of $F(p)$ into a MacLaurin series, in the form

$$d_n = \sum_{m=0}^{n-1} (-1)^{n-m} C_{n-1}^m \lambda^{n-m} S_{n-m} \quad (12)$$

The entire process is illustrated by several examples of decomposition of $F(p)$ as a function of $f(t)$ and of parameter-dependent forms into a Burman-Lagrange series and by the characterization of several actual engineering problems. There are 2 figures.

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Application of the Burman-Lagrange....

ASSOCIATION:

Institut avtomatiki i elektrometrii Sibirskogo
otdeleniya AN SSSR, Novosibirsk (Institute of
Automation and Electrical Measurements, Siberian
Section of the AS USSR, Novosibirsk)

SUBMITTED:

July 5, 1961

Card 3/3

DEVYATOV, B.N.

Application of a special system of polynomials to the approximation
of the transition process in an infinite interval. Izv. SO AN SSSR
no.2 Ser. tekhn. nauk no.1:46-50 '63. (MIRA 16:8)

1. Institut avtomatiki i elektrometrii Sibirskogo otdeleniya
AN SSSR, Novosibirsk.
(Polynomials)

DEVYATOV, B.N.; GIMEL'SHEYN, F.Ya.; KHOR'KOVA, G.S.

Using distributed control for creating high-quality control systems
for technological processes of heat and mass transfer. Izv. SO
AN SSSR no.2 Ser. tekhn. nauk no.1:60-77 '63. (MIRA 16:8)

1. Institut ~~avtomatiki~~ i elektrometrii Sibirskogo otdeleniya
AN SSSR, Novosibirsk.
(Heat—Transmission) (Mass transfer)
(Automatic control)

DEVYATOV, B.N.

Synthesis of invariant systems for controlling distributed processes of chemical technology. Dokl. AN SSSR 150 no.3:
612-615 My '63. (MIRA 16:6)

1. Institut avtomatiki i elektrometrii Sibirskogo otdeleniya
AN SSSR. Predstavлено академиком V.S. Kulebakиным.
(Chemical engineering)

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BOOK EXPLOITATION

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BT1

Deryatov, Boris Nikolayevich

The theory of transient processes in technological devices from the point of view of problems of control (Teoriya perekhodnykh protsessov v tekhnologicheskikh apparaatakh s tekhnicheskimi zadachami upravleniya) Nauksgiz, Redizdat, izdel. Sibirs. izdel. AN SSSR, 1964. 332 p. illus., bibli. Errata slip inserted. 1800 copies printed. (At head of title: Akademiya nauk SSSR, Sibirske st-deleniye) Editor: G. N. Laderin; Technical editors: T. K. Ovchinnikova, O. A. Lekshina; Proofreaders: T. P. Sabina, Ye. P. Sharabarin.

TOPIC TAGS: absorber, chemical engineering, continuous process, counterflow, direct flow, extractor, heat exchange, heat treating furnace, mass exchange, rectification column, scrubber, transient process

PURPOSE AND COVERAGE: This monograph is devoted to the theoretical investigation of the dynamic characteristics of the technological processes of heat and mass exchange achieved by the principle of counterflow or of direct flow in moving media. The purpose of the book is to formulate a general linear theory of tran-

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sient processes that are characteristic for a wide class of typical technological devices, including heat exchangers, absorbers, scrubbers, extractors, rectification columns, heat-treating furnaces, and others. Herein, general methods are given for analyzing the dynamics of the processes. Only the basic characteristics of the dynamics of counterflow processes are considered. The question of transients is investigated in order to clarify the dependence of the reaction of a device to a disturbance of stationary conditions on its parameters and operating conditions. Two possible methods of analyzing nonstationary problems are described, both for multistage devices and for devices of the continuous type with direct- and counterflow of the medium. The first method utilizes the device of ordinary differential equations, and the second, equations with partial derivatives. The basic material for this monograph was work performed under the author's direction for the last 10 years at the Ural'skiy Naukno-Issledovatel'skiy Institut Khimii and in the Institut Avtomatiki i Elektronmetrii Sibirskego Otdeleniya AN SSSR.

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L 27390-65
AM5003783

Ch. XI. Synthesis of control systems for technological processes with utilization of distributed control -- 293
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SUB CODE: CG SUBMITTED: 11Jul64 NR REF Sov: 088
OTHER: 016

Card 4/4

"APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0

DEVYATOV, B.N.; CHEBOTAYEV, P.Z.

Transient modes of continuously operating industrial apparatus.
Trudy Inst. avtom i elektrometr. SO AN SSSR no.8:63-79 '64.
(MIRA 17:11)

APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0"

DEVYATOV, B.N.; KHOR'KOVA, G.S.

Analysis of the dynamic characteristics of counterflow-type
industrial processes taking into account change in the speed
of the media. Trudy Inst. avtom. i elektrometr. SO AN SSSR
no.8:80-92 '64. (MIRA 17:11)

GIMEL'SHTEYN, F.Ye.; DUVIATOV, B.N.

Problem of optimal estimation of the state of controlled
chemical production processes. Dokl. AN SSSR 165 no.2:366.
371 N '65. (MIRA 18:11)

1. Institut avtomatiki i elektronika Sibirskego otdeleniya
AN SSSR. Submitted April 20, 1965.

DEVYATOV, D. S.

Podshipnik kachenija sovetskikh avtomobilei [Antifriction bearings in Soviet automobiles]. Moskva, Izd-vo MKhR RFSR, 1953. 248 p.

SO: Monthly List of Russian Accessions, Vol. 6 No. 11 February 1954

DEVYATOV, F.F., master reostatnykh ispytaniy

Checking the current limiter of the network of the main generator.
Elekt. i teplo. tsiaga 5 no. 10:30-31 0 '61. (MIRA 14:10)

1. Tashkentskiy teplovozovagonoremontnyy zavod.
(Diesel locomotives--Inspection)

DEVYATOV, G.; ISAYEV, Ye.

Scientific production conferences on problems of production
organization and utilization of its potentials. Vop. ekon. no.10:
134-136 O '59, (MIRA 12:12)
(Siberia--Industrial organization)

L11167-56 EWT(1)/EWT(m) JD

ACC NR: AP6000366

SOURCE CODE: UR/0286/65/000/021/0061/0061

AUTHORS: Devyatov, G. K.; Levit, M. Ye.; Ivanov, V. I.; Kostomakhin, V. A.;
Medzhitov, R. D.

44

44

44

44

41
QB

ORG: none

TITLE: Device for contactless measurement of rotor sag. Class 42, No. 176106
[announced by Moscow Order of Lenin Aviation Institute, im. Sergo Ordzhonikidze
(Moskovskiy ordena Lenina aviatziionnyy institut)]

SOURCE: Byulleten' izobreteniij i tovarnykh znakov, no. 21, 1965, 61.

TOPIC TAGS: electronic circuit, detection equipment

ABSTRACT: This Author Certificate presents a device for contactless measurement of rotor sag. The device contains a capacitive unary sensor included in a resonance circuit supplied by a high frequency oscillator, a detector, and a matching stage with a meter (see Fig. 1). To simplify the measuring process and to increase the readout accuracy, a compensating capacitor is inserted in the resonance circuit in series with the sensor. The capacitor insures a linear dependence between the magnitudes of the output voltage and rotor sag.

Corr: 1/2

UDC: 531.717.2:621.317.39

L 11167-66

ACC NR: AP6000366

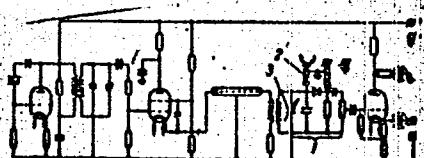


Fig. 1. 1 - Resonance circuit;
2 - sensor; 3 - compensating capacitor.

Orig. art. has: 1 diagram.

SUB CODE: 09/ SUBM DATE: 17Jul64

AC
Card 2/2

DEVYATOV, G.S.

Increasing the effectiveness of mining systems used in the
Prokop'yevsk-Kiselevsk deposit region of the Kuznetsk Basin,
Izv. Sib. otd. AN SSSR no.1:71-81 '58. (MIRA 11:8)

1.Zapadno-Sibirskiy filial AN-SSSR.
(Prokop'yevsk region--Coal mines and mining)
(Kiselevsk region--Coal mines and mining)

PRUDENSKIY, G.A., red.; SOMINSKIY, V.S., otv. red.; BELOUSOVA, V.S.,
red.; DEVYATOV, G.S., red.; ISAYEV, Ye.H., red.; MEKKEL',
S.A., red.; CHERKASOV, G.N., red.; KUPAYEVA, L.A., red.;
MAZUROVA, A.F., tekhn. red.; VYALYKH, A.M., tekhn. red.

[Potentials of working time in the industries of Siberia] Rezervy rabochego vremeni v promyshlennosti Sibiri. Pod obshchey red. G.A. Prudenskogo. Novosibirsk, Izd-vo Sibirskogo otd-niya AN SSSR, 1961. 221 p. (MIRA 15:8)

1. Akademiya nauk SSSR. Sibirskoye otdeleniye. Institut ekonomiki i organizatsii promyshlennogo proizvodstva.
(Siberia--Labor productivity)
(Siberia--Time study)

PEREVOZCHIKOV, B.S.; SANNIKOV, S.S.; PASMANIK, A.I.; Prinimali
uchastie: PROTOPOPOVA, T.I.; POLOSHAKOV, Yu.A.; KOROLEV,
V.O.; TROSTYANITSER, G.N.; TVERSKIY, G.A.; DEVYATOV, I.I.

Adjustment of low-flash forging on a 4000-ton, NEKZ crankshaft
hot forging press. Kuz.-shtam. proizv. 3 no.8:41-43 Ag '61.

(MIRA 14:8)

(Forging) (Power presses)

BOLOTIN, Yu.A.; DEVYATOV, I.Kh.

Air drilling. Razved. i okh. nedr 29 no.11:49-51 N '63.
(MIRA 17:12)
1. Bashkirskoye geologicheskoye upravleniye.

84605

1.3300 only 2208, 2708

S/135/60/000/004/002/008
A115/A029

AUTHORS: Shablygin, S.V., Candidate of Technical Sciences, Devyatov, I.M.,
Engineer

TITLE: Battery Supplied Contact Welding

PERIODICAL: Svarochnoye proizvodstvo, 1960, No. 4, pp. 8 - 9

TEXT: By order of the VNIIESO (All-Union Scientific Research Institute of Electric Welding) the SADI (Saratov Automobile and Highway Institute) developed a point-welding apparatus using 10 - 20,000 amp lead-acid or alkaline batteries. Characteristics of nickel-iron laminated, cadmium-nickel non-laminated, and lead-acid aircraft batteries were tested. The 6-CAM-55(6-SAM-55) lead-acid aircraft battery of 370x185x165 mm size, 20 kg weight and 12 v, has been found most suitable and was improved by I.M. Devyatov. (Fig. 1). Half-blocks of the same polarity were connected by massive copper bars covered by a lead cover with copper pipes in it for water cooling. The 6-SAM-55 battery blocks 1 and 2 have been used and the ribs were eliminated. The electrolyte was cooled sufficiently and the temperature did not exceed 40°C. The capacity of the new SAM-330 battery, is 330 amp-h. Figure 2 shows the temperature curves under a working discharge of 6000

Card 1/3

84605

S/135/60/000/004/002/008
A115/A029

Battery Supplied Contact Welding

amp. A water-cooled graphite circuit breaker (Figure 4) has been used. The clearance between the graphite contacts does not exceed 1 mm which allows for 200 switchings per minute. During tests, the contactor performed about 200,000 breakings without any damage to the graphite surface. Two battery sets for spot welding of 1+1 mm steel, and for welding of 4+4 mm plates and 0.8+0.8 mm aluminum alloys have been designed. Characteristics of the battery sets are given in a table. The batteries were coupled with an ATP-25 (ATP-25) generator by a flexible cable. The characteristics of the generator are: 12/6 v, 750/1,500 amp, 1,420, rpm. The relatively high internal resistance of the generator makes possible continuous charging during the welding process. Working conditions are: welding 0.2 sec, welding current 6,000 amp, intervals 1.8 sec. The voltage of the generator during the interval was 7.8 v and during the welding process 6.4 v at 600 and 1,640 amp. The voltage of the generator has been selected so as to enable it to be charged during the interval and to replace the loss by discharge. Oscillograms of welding current and voltage are given in Figure 5. Battery welding units will find wider application in special instances of resistance welding, if batteries with sufficient term of service will be developed. There are 5 figures and 1 table.

Card 2/3

84605

S/135/60/000/004/002/008
A115/A029

Battery Supplied Contact Welding

ASSOCIATION: Saratovskiy avtomobil'no-dorozhnyy institut, SADI (Saratov Highway Institute).

X

Card 3/3

DEVYATOV, M.V. (shkola Kazani); NIKITIN, I.V.; GORSHENKOV, N.G.;
RUTKOVSKIY, O.O. (Alma-Ata); DAVYDOV, A.V.; LEBEDEVA, G.P.

Letters to the editor. Geog. v shkole 21 no.5:72-75 S-0
'58. (MIRA 11:10)

1. Shkola No.5 g.Selnechnogorska (for Nikitin). 2. Takhromskaya
shkola Moskovskoy oblasti (for Gorshenkov). 3. Vikulovskaya shkola
Tyumenskoy oblasti (for Davydov). 4. Ul'yanovskaya shkola Kaluzhskoy
oblasti (for Lebedeva).

(Geography--Study and teaching)

DEVYATOV, N.M.

Course of pregnancy and labor following pulmonary resection. Zdravookhranenie 3 no.6:56-57 N-D '60. (MIRA 13:12)

1. Iz kafedry akusherstva i ginekologii (zav. - prof. A.Z.Kocherginskiy)
Kishinevskogo meditsinskogo instituta.
(LUNGS—SURGERY) (PREGNANCY)

DIEVYATOV, N.M.

Course of pulmonary tuberculosis following an abortion at
different periods of pregnancy. Trudy Kish.gos.med.inst.
13:179-182 '60. (MIRA 16:2)

1. Kafedra akusherstva i ginekologii Kishinevskogo gosudarst-
vennogo meditsinskogo instituta.
(TUBERCULOSIS) (ABORTION)

POPOVA, T.A., dotsent; DEVYATOV, N.N., dotsent [deceased]

So-called epiphyseal osteomyelitis in young children. Khirurgia 39 no.4:124-128 Ap'63
(MIRA 17:2)

1. Iz kafedry detskoy khirurgii (zav. - prof. A.F. Zverev) i
kafedry rentgenologii (zav. - dotsent N.N.Devyatov [deceased])
Sverdlovskogo meditsinskogo instituta.

DEVYATOV, V., nauchnyy sotrudnik.

Complete defeat of Kornilov. Sov.mor. 17 no.17:5 S '57. (MIRA 10:10)

1. Musey Revolyutsii SSSR.
(Russia--Revolution, 1917-1921)

"APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0

DEVJATOV, V.

Patent library. NTO 3 no.3:58-60 Mr '61.
(Engineering libraries) (Patents)

(MIRA 14:3)

APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0"

KOSTYLEV, S.A., inzh.-geolog; DEYYATOV, V.G., inzh.-gidrotekhnik; SPASOLOMSKIY,
V.V.; SYUNDYUKOV, G.M., dotsent, kand. tekhn. nauk

Deformations in the structures of buildings caused by inadmissible
settling of foundations, and the reasons for their origin. Sbor.
trub. Inzh.-stroi. fak. Chel. politekh. inst. no.3:183-198 '63.
(MIRA 17:9)

1. Glavnnyy inzh. proyekt'nogo instituta Chelyabinskgorproyekt (for
Spasolomskiy).

L 13636..66 EWT(1)/EWT(m)/ENP(w)/ENP(r)/T-2/ENP(k)/ETC(m) JD/EM
ACC NR: AR5025455 SOURCE CODE: UR/0285/65/000/008/0015/0015

SOURCE: Ref. zh. Turbostroyeniye, Abs. 8.49.106

AUTHOR: Devyatov, V. I.

TITLE: A study of certain variants of air cooling the turbine disks

CITED SOURCE: Tr. Kazansk. aviat. in-ta, vyp. 86, 1964, 84-97

TOPIC TAGS: turbine, turbine cooling, turbine blade, heat transfer, heat tolerance

TRANSLATION: Thermal tests were conducted for the purpose of comparing means of cooling turbine disks. The construction of an experimental set-up is described. As a result of the tests it was shown, that one-sided peripheral blowout under forced cooling air at an angle of 90° with the disk is most effective. This method is least sensitive to variation in the disk rpm and produces the best results both at the periphery and in the center of the disk. Among the reflector cooling devices the most effective is the type with air fed underneath the deflector, and with the subsequent air outflow through the artificial notches in the blade base. All deflector mechanisms are very sensitive to variation in rpm and less sensitive to variation in the flow of cooling air.

SUB CODE: 10/

Card 1/1 Hw)

UDC: 621.438

DEVYATOV, V.K.

Twenty-fifth anniversary of the L.M.Kaganovich First State Bearing
Plant. Mashinostroitel' no.4:5-7 Ap '57. (MLRA 10:5)

1.Zamestitel' ministra avtomobil'noy pro-vshlennosti Soyusa SSR.
(Moscow--Bearing industry)

SOLOV'TSEV, N.S.; DEVYATOV, V.V.

Stamping of parts by the method of extrusion rolling. Trakt. i
sel'khozmash. no.11:35-37 N '64. (MIRA 18:1)

L. Nauchno-issledovatel'skiy institut tekhnologii traktornogo i
sel'skokhozyatstvennogo mashinostroyeniya.

ZIMKIN, Ye.A.; KLYUCHEVICH, V.P.; DREVYATOV, Ya.E.; P'YANKOVA, L.N.;
GARANTINA, Ye.Ye.

Effect of the methods of gelatin preparation on its photographic
activity. Zhur. nauch. i prikl. fot. i kin. 30 no.4:247-250
Jl-Ag '65.
(MIRA 18:7)

I. Kazanskiy filial Vsesoyuznogo nauchno-issledovatel'skogo kine-
fotoinstituta i Kazanskiy fotofilmotekhnicheskiy zavod.

ZIMKIN, Ye.A.; DEVYATOV, Ya.B.; MAKLAKOV, A.G.

Carbohydrates in collagen and gelatin. Reducing the duration of
liming. Zhur.prikl.khim. 38 no.11:2581-2585 N '65.

(MIRA 18:12)

2. Kazanskiy filial Vsesoyuznogo nauchno-issledovatel'skogo
kinofotoinstituta i kazanskiy zhelatinevyy zavod. Submitted
August 15, 1964.

"APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0

DEVYATOV, YA. B.; ARBUZOV, B.A.; ABRAMOV, V.S.

"The Products of Condensation of Cyclones with p-Benzoquinone and Naphthoquinone",
Zhur. Obshch. Khim., 9, No. 17, 1939. Laboratory of Organic Chemistry, Kazan'
Chemico-Technological Institute imeni S. M. Kirov. Rec'd 22 Feb 1939. (PP 1D59-1563).

■ Report U-1614, 3 Jan 1952.

APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0"

DEVIATOVA, A.P.; MIKHAYLOVA, O.A.; YAKUNINA, T.I.

Isolation of the causative agent of pseudotuberculosis from
gray and white rats in Vladivostok. Izv. Irk.gos.nauch.-issl.
protivoochum.inst. 20:303-305 '59. (MIRA 13:7)
(VLADIVOSTOK--PATMURELLA PSEUDOTUBERCULOSIS)

DEVYATOVA, A. P., KHUNDANOV, L. E., and SHKURKO, E. D.

"Gamma-globulin in Experimental Anthrax Infection."

Veterinariya, Vol. 38, No. 6, 1961. p 45

Irkutsk Sci. Res. Inst, Min. Public Health USSR (Devyatova, A. P.)

KHUNDANOV, L.Ye.; DEVYATOVA, A.P.; PADALKO, Z.F.; LUK'YANOVA, V.I.;
SHKURKO, Ye.D.

Comparative study on the effectiveness of antibiotics and γ -globulin
in experimental melioidosis. Zhur. mikrobiol. epid. i immun. 32 no.7:
114-117 Je '61.
(MIRA 15:5)

1. Iz Irkutskogo gosudarstvennogo nauchno-issledovatel'skogo
protivochumnogo instituta Sibiri i Dal'nego Vostoka.
(MELOIDOSIS) (ANTIBIOTICS)
(GAMMA GLOBULIN)

KHUNDANOV, L.Ye.; SHKURKO, Ye.D.; DEVYATOVA, A.P.

Gamma globulin in experimental anthrax infection. Veterinarija 38
no.6:45-46 Je '61. (MIRA 16:6)

1. Irkutskiy nauchno-issledovatel'skiy institut Ministerstva
zdravookhraneniya SSSR.

(Gamma globulin) (Anthrax)

L 20313-66 EWT(1)/T JK

ACCESSION NR: AP5011269

UR/0016/65/000/004/0012/0013

AUTHOR: Khveshchenko, Ye. N.; Padalko, Z. F.; Devyatova, A. P.;
Rodionova, A. P.; Mirotvortsev, Yu. I.; Mirgorodskiy, N. T. //

TITLE: Tularemia detection in Primorskiy kray

SOURCE: Zhurnal mikrobiologii, epidemiologii i immunobiologii,
no. 4, 1965, 12-13

TOPIC TAGS: man, tularemia, Primorskiy kray, serologic test,
natural focus, rodent, tick

ABSTRACT: The first case of tularemia in Primorskiy Kray was reported in 1963 in the Ussurisk district, but no evidence of tularemia natural foci has been found to date by the Primorskiy Antiplague Station. On the basis of clinical symptoms, the case of a 56 yr old patient, a native of the area, was diagnosed as an eye-bubonic form of tularemia. The patient's tularin intradermal test proved positive and agglutination reaction was markedly positive with a titer of 1:400. A tularemia culture was not isolated. The patient was hospitalized in an infectious disease hospital and treated with

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L 20313-66

ACCESSION NR: AP5011269

streptomycin. The patient was reexamined 3 mos after recovery at which time the agglutination reaction titer was 1:3200. It is assumed that the infection was transmitted through the water of the Lyuchikheza River in which the patient frequently washed. Intradermal tularin tests administered to village residents disclosed positive reactions in 18 persons, two of whom may be considered infected. The presence of various rodents and ticks in the area indicate that the extensive bacteriological investigation of the Antiplague Station should be continued to determine the natural foci of tularemia.
Orig. art. has: None.

ASSOCIATION: Primorskaya krayevaya protivochumnsaya stantsiya
(Primorskiy Kray Antiplague Station)

SUBMITTED: 02Mar64

ENCL: 00

SUB CODE: LS

NR REF SOV: 000

OTHER: 000

Card 2/2 BK

3(0)

AUTHOR: Devyatova, E. I.

SOV/20-125-1-44/67

TITLE: Marine Interglacial Deposits in the Basin of the
Onega River (Morskiye mezhdinikovyye otlozheniya
basseyyna r. Onegi)

PERIODICAL: Doklady Akademii nauk SSSR, 1959, Vol 125, Nr 1,
pp 162-165 (USSR)

ABSTRACT: In the Onega River region towards the end of the
interglacial marine transgression, the relief of the
bedrock cover was carved into a network of erosion valleys
and depressions. Thus the variation in the vertical
distribution and the restriction of the interglacial
sediments are dependent on the old form of the relief.
The thickness of the sediments varies between 1.5 and 45 m.
The author describes these sediments together with their
fauna and flora remains along the rivers Tyolza, Somba,
Tyoksa and Iksa as well as along the upper Mosha. They
indicate that sublitoral, primarily arctic and arctic-
boreal conditions prevailed. On the other hand, only a
few littoral species are found in the faunal complex of the
coastal zone. Arctic species are found only singly. Warm

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Marine Interglacial Deposits in the Basin of the
Onega River

SOV/20-125-1-44/67

water molluscs had not at that time achieved a wide distribution and were only associated with local, well-warmed water. In deeper ocean regions a temperate faunal complex developed. Among the diatoms are marine, primarily sublitoral benthic diatom species; neritic plankton species are sparse. Also the diatom flora belong with respect to temperature, to a temperate boreal cold-water type, including a few warm-water types. According to their stratigraphic position as well as the fauna and diatom flora association, the Onega River sediments belong to the boreal transgression of the Dnepr-Valday (dneprisko-valdayskoye) Interglacial Period. The spore-pollen diagrams confirm these findings. The data obtained in this line facilitated comparison with the diagrams of core borings of the European Plain. From this the following general sequence of vegetation development could be determined. During the climatic optimum, the consecutive high points (maximum growth periods) of oak (*Quercus*), elm (*Ulmus*), and hornbeam birch (*Carpinus*) follow one another. Following the climatic cooling towards the end of the interglacial period,

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Marine Interglacial Deposits in the Basin of the
Onega River

SOV/20-125-1-44/67

deciduous trees were replaced by light-needled forests, then dark-needled forests. The interglacial sediments here have a uniform character. A colder and younger Onega (onezhskaya) transgression could not be differentiated. During the last Valday (valdayskoye) glacial advance the whole region under discussion was covered with ice. The edge of the ice was east of this space. No clues of a younger glacial advance have been found. There are 2 figures and 3 Soviet references.

ASSOCIATION: Komi-filial Akademii nauk SSSR (Komi Branch, Academy of Sciences, USSR)

PRESENTED: October 6, 1958, by V. N. Sukachev, Academician

SUBMITTED: October 5, 1958

Card 3/3

DEVYATOVA, Eleonora Ivanovna; MARKOV, K.K., doktor geogr. nauk, prof.,
otv. red.; IVENSEN, Yu.P., doktor geol.-mineral. nauk, otv.
red.; SHENGER, I.A., red. izd-va; ZENDEL', M.Ye., tekhn. red.

[Stratigraphy of Quaternary sediments and paleogeography of the
Quaternary period of the Onega basin] Stratigrafiia chetver-
tichnykh otlozhenii i paleogeografiia chetvertichnogo perioda v
basseine reki Onegi. Moskva, Izd-vo Akad. nauk SSSR, 1961. 88 p.
(MIRA 14:8)

(Onega Valley—Paleogeography) (Onega Valley—Geology, Stratigraphic)

DEVYATOVA, E.I.

Stratigraphy of Quaternary sediments in the western part of the
Timan Ridge region. Trudy Inst.geol.Komi fil. AN SSSR no.3:
103-112 '62. (MIRA 16:9)
(Timan Ridge region--Geology, Stratigraphic)

DEVYATOVA, E.I.

Marginal formations of the Valday Glacier in Archangel Province.
Trudy Kom. chetv. per. 21:21-29 '63. (MIRA 16:10)

1. Komi filial AN SSSR.

DEVYATOVA, E.I.; LOSEVA, E.I.; CHERNOV, A.A., doktor geol.-min.
nauk, prof., ctv. red.[deceased]; VARSANOF'YEVA, V.A.,
red.; VISKE, G.S., red.

[Stratigraphy and paleogeography of the Quaternary of the Me-
zei Basin] Stratigrafiia i paleogeografiia chetvertich-
nogo perioda v basseine r. Mezeni. Leningrad, Nauka,
1964. 104 p. (MIRA 17:9)

DEVYATOVA, L.N.

Problem of the treatment of carriers of *Corynebacterium diphtheriae*.
Zhur.mikrobiol., epid. i immun. 27 no.8:39-42 Ag '56. (MLRA 9:10)

1. Iz kafedry epidemiologii TSentral'nogo instituta usovershenstvovaniya vrachey.

(DIPHTHERIA, prevention and control,
penicillin (Rus))

(PENICILLIN, therapeutic use,
diphtheria prev. (Rus))

DEVYATOVA, L.N.

Results of treating diphtheria with penicillin tablets and aerosols.
Zhur.mikrobiol.epid. i immun. 27 no.9:86-90 S '56. (MLRA 9:10)

1. Iz kafedry epidemiologii TSnetral'nogo instituta usovershenstvovaniya vrachey.

(DIPHTHERIA, prevention and control,
penicillin aerosols & tablets (Rus))

(PENICILLIN, therapeutic use,

diphtheria prev., tablets & aerosols (Rus))

(AEROSOLS, therapeutic use,

penicillin in diphtheria prev. (Rus))

Devyatova, L.N.

DEVYATOVA, L.N.

Epidemiological observations in centers of dysentery infection.
Zhur.mikrobiol.epid. i immun.,supplement for 1956:20-21 '57

1. Iz Tsentral'nogo instituta usovremenstvovaniya vrachey.
(DYSENTERY)

USSR / Microbiology. Microbes Pathogenic for Man and Animals. Bacteria. Root Bacteria. F-4

Abs Jour: Ref Zhur-Biol., 1958, No 17, 76806.

Author : Devyatova, L. N.
* Inst : Not given.

Title : On the Problem of Clinical and Bacteriological Characteristic of Carriers of the Diphtheria Rod.

Orig Pub: Zh. mikrobiol., epidemiol. i immunobiol., 1957,
No 12, 48-53.

Abstract: No abstract.

* Iz KAFEDRY EPIDEMIOLOGII TSENTRAL'NOGO INSTITUTA VSOVERSHENSTVOVANIYA
VRACHENIY.

Card 1/1

50

"APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0

DEVYATOVA, L.N.

BENLIKOV, G.P.; DEVYATOVA, L.N.

First All-Russian Conference of Epidemiologists, Microbiologists
and Specialists in Infectious diseases. Zdrav. Ros.Feder. 2 no.1:
45-47 Ja '58. (MIRA 11:2)
(EPIDEMIOLOGY) (MICROBIOLOGY)
(COMMUNICABLE DISEASES)

APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0"

HELIKOV, G.P., DEVYATOVA, L.N.

Expanded plenary session of the administration of the All-Russian
Medical Society of Epidemiologists, Microbiologists and Specialists
in Infectious Diseases. Zdrav.Ros.Feder. 2 no.11:45-47 N '58

(MIRAll:12)

(COMMUNICABLE DISEASES)

DEVYATOVA, L.N.

Variability of *Corynebacterium diphtheriae*; data on epidemiological observations. Zhur.mikrobiol.epid. i immun. 29 no.5:88-90 My '58
(MIRA 11:6)

1. Iz kafedry epidemiologii TSentral'nogo instituta usovershenstvovaniya vrachey.

(CORYNEBACTERIUM DIPHTHERIAE,
variability (Rus))

DEVYATOVA, L.N.; MYASNIKOV, Yu. A.

"Life and death of epidemics" by M.G. Gol'din. Zhur. mikrobiol. epid.
i immun. ?9 no. 12:118-120 D '58. (MIRA 12:1)
(EPIDEMICS)

DEVYATOVA, L.N.; HELIKOV, G.P.

Organization activities of the administration and local chapters
of the All-Russian Medical Society of Epidemiologists, Microbi-
ologists, and Specialists in Infectious Diseases, 1958-1959 D '59.
(MIRA 13:5)
(BACTERIOLOGICAL SOCIETIES)

DEVYATOVA, L.N.

Active immunization and means for its realization in Great Britain.
Zhur. mikrobiol. epid. i immun. 31 no.2:33-37 D '60.

(MIRA 14:6)

1. Iz kafedry epidemiologii TSentral'nogo instituta usovershenstvovaniya vrachey.

(GREAT BRITAIN—VACCINATION)

DEVYATOVA, L.N.

Current data concerning the world-wide distribution of ornithosis.
Trudy TSIU 68:43-48 '64. (MIRA 18:5)

"APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0

BUZDENENKHOV, I.S.; DEVYATOVA, L.N.; NELYUBOV, I.D.

Analysis of the occurrence of ornithosis in the U.S.S.R.
Trudy TSU 80:26-24 '65. (MTR4 18:11)

APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0"

DEVYATOVA, N. I.

USSR/Chemistry - Synthesis

Card 1/1 : Pub. 151 - 31/42

Authors : Slobodin, Ya. M.; Blinova, M. V.; and Devyatova, N. I.

Title : Synthesis of cyclopentanol

Periodical : Zhur. ob. khim. 24/9, 1639-1640, Sep 1954

Abstract : Various methods of reducing cyclopentanol were investigated. It was established that hydrogenation of cyclopentanol, over a Ni-catalyst applied on diatomaceous earth (kieselguhr) at 125°, results in formation of cyclopentane. The results obtained, during hydrogenation over a copper-chromium-barium catalyst at 160-170°, are described. Eight references: 3-German; 2-USSR; 2-French and 1-USA (1893-1944).

Institution : ...

Submitted : April 14, 1954

5.3010

10377
SOV/70-30-5-29/69

AUTHORS: Ioffe, I. S., Devyatova, N. I.

TITLE: N-Substituted Amides of Salicylic Acid and Its Derivatives. II. Meso-Acridylamide of Salicylic Acid

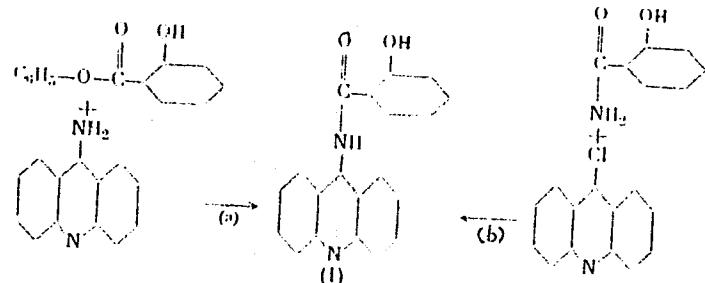
PERIODICAL: Zhurnal obshchey khimii, 1960, Vol 30, Nr 3, pp 884-889 (USSR)

ABSTRACT: The reaction of salol with meso-aminoacridine yields a mixture of products from which the following three were identified: salicylic salt of meso-aminoacridine, mp 279-280°; meso-acridylamide, (I), mp 267-268°; and di-(meso-acridyl)-amine, mp 360°. The structure of (I) was confirmed by its synthesis from meso-chloroacridine and amide of salicylic acid according to scheme (b).

Card 1/5

N-Substituted Amides of Salicylic Acid and Its Derivatives. II

78275
SOV/79-30-3-29/69

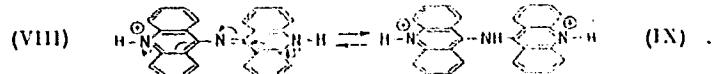
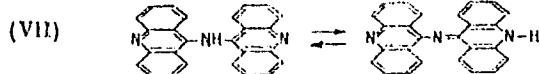


Di-(meso-acridyl)-amine forms with acids bright-red onium salts. This amine is formed as a result of secondary reaction of the formed amide with meso-aminoacridine. The structure of di-(meso-acridyl)-amine (VII) was confirmed by its synthesis from meso-chloroacridine and meso-aminoacridine. The color of this amine can be explained by possible tautomerism in its acridine rings resulting in acridoneimine structure.

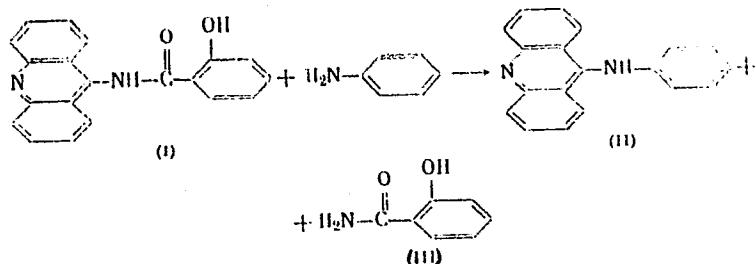
Card 2/5

N-Substituted Amides of Salicylic Acid and Its Derivatives. II

78275
SOV/79-30-3-29/69



Meso-acridylamide of salicylic acid (I) reacts with other amines with elimination of salicylamide (III) and formation of corresponding substituted meso-aminoacridine (II)

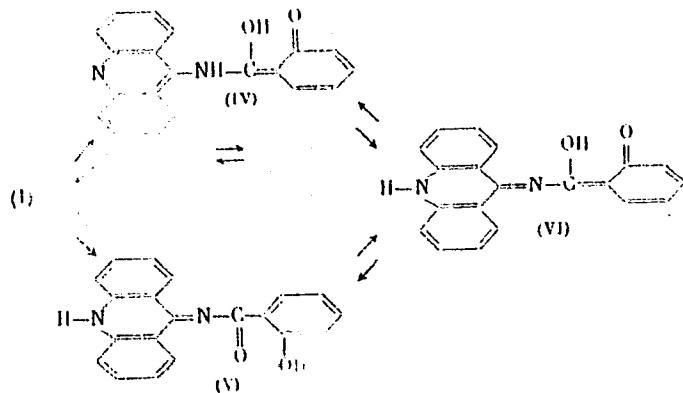


Card 3/5

N-Substituted Amides of Salicylic Acid and Its Derivatives. II

78275
SOV/79-30-3-29/69

The authors explain the instability of the bond between nitrogen atom and meso-carbon of the acridine ring in acridylamine of salicylic acid by the mutual effect of both groups of this compound. The bright yellow color of this acyl derivative can be also explained by this phenomenon.



Card 4/5

N-Substituted Amides of Salicylic
Acid and Its Derivatives. II

78275
SOV/79-30-3-29/69

There are 4 references, 1 Soviet, 2 U.K., 1 U.S. The
U.S. and U.K. references are: Allen, C. T., Van Allen,
J. A., Org. Snyth., 26, 92 (1946); Albert, A., Bruce
Ritchil, J. Chem. Soc., 458 (1943); Dupre, D. I.,
Robinson, T. A., J. Chem. Soc., 549 (1945).

SUBMITTED: March 11, 1959

Card 5/5

TOFFE, I.S.; DEVYATOVA, N.I.; ROSKULYAK, L.A.

Sulfonic acids of fluorescein. Part 1: Condensation of
sulfophthalic acids with resorcinol. Zhur. ob. khim. 32 no.7:2107-
2111 Jl '62.
(Phthalic acid) (Resorcinol)

IOFFE, I.S.; DEVYATOVA, N.I.

Sulfonic acids of fluorescein. Part 2: Preparation of sulfophthalic acids. Zhur. ob. khim. 32 no.7:2111-2115 Jl '62. (MIRA 15:7)
(Phthalic acid) (Fluorescein)

DEVYATOVA, N.I.

N-acyl derivatives of p-aminosalicylic acid containing residues
of cycloalkanecarboxylic acids. Zhur. ob. khim. 32 no.5:1710-1711
My '62. (MIRA 15:5)
(Salicylic acid) (Acids, Organic)

"APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0

IOFFE, I.S.; DEVYATOVA, N.I.; GOFMAN, I.A.

Rhodamine dyes and related compounds. Part 9: Sulfonic acids of
rhodamine B and their derivatives. Zhur.ob.khim. 34 no.2:640-644
F '64. (MIRA 17:3)

APPROVED FOR RELEASE: 06/12/2000

CIA-RDP86-00513R000410310011-0"

DEVYATOVA, N.I.

Carrier state of diphtheria. Report No.1: Dynamics of the diphtheria carrier state under varicous epidemiological conditions. Zhur. mikrobiol., epid. i immun. 41 no.9:3-8 S '64. (MIRA 18:4)

1. Moskovskiy institut vektsin i syvorotok imeni Mechnikova.

DEVYATOVA, N.K., inzh.

Thermal properties of large-panel apartment houses with walls made
of cellular concretes. Issl.po mikroklim.nasel.mest i zdan. i po
stroi.fiz. no.2:124-140 '62. (MIRA 16:6)

1. Ural'skiy nauchno-issledovatel'skiy institut Akademii
kommunal'nogo khozyaystva im. Pamfilova RSFSR.
(Sverdlovsk--Walls--Thermal properties)
(Lightweight concrete)

DEVYATOVA, V. A.

DEVYATOVA, V. A.—"Aerological Peculiarities of the Bottom Kilometer Layer of the Atmosphere." (Dissertation for Degrees in Science and Engineering* Defended at USSR Higher Educational Institutions) Main Administration of the Hydrometeorological Service Attached to the Council of Ministers USSR, Central Inst of Forecasts, Moscow 1955* Geographical Sciences

SO: Knizhnaya Letopis' No. 37, 10 September. 1955.

DEVYATOVA, Valentina Alekseevna; PINUS, N.Z., otvetstvennyy redaktor;
VLASOVA, Yu.V., redaktor; BRAYNINA, M.I., tekhnicheskiy redaktor;

[Microaerological studies of the lower kilometric layer of the
atmosphere] Mikroaerologicheskie issledovaniia nizhnego kilometro-
vogo sloia atmosfery. Leningrad, Gidrometeo.izd-vo, 1957. 143 p.
: (MLRA 10:5)
(Atmosphere)

DEVYATOVA, V.A.; PYATYSHEV, R.V.; TYDEL'SKAYA, R.O.; CHERENKOVA, I.A.

Studying pulsations of the horizontal component of the velocity
of winds up to an altitude of 5 kilometers. Trudy TSAO no.21:
52-175 '58. (MIRA 11:11)

(Winds)